



Gesellschaft für Anlagen-  
und Reaktorsicherheit  
(GRS) gGmbH

## **ATHLET 3.3**

### **Program Updates**







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## About this Document

The ATHLET Program Updates Manual lists the major program modifications and patches to the current ATHLET code version. It provides information not only for the ATHLET users but also for the developers, i.e. it may contain details which are not relevant for 'normal' code users.

Further information on program modifications relevant for ATHLET applications can be found under Document Updates in the *User's Manual* as well as under Input Data Updates in the *Input Data Description*.

**On ATHLET patches:** Although ATHLET is comprehensively tested and validated before it is released, program errors or weaknesses cannot be completely avoided. There are several reasons for that:

- The test cases we use don't cover the whole range of applicability of ATHLET.
- We cannot foresee all the possible errors that could occur when the program is applied.
- Novel applications may require new models, changes in proper use of models, or adjusted or extended input and run time checks.
- User feedback may indicate needs of program modifications.
- Despite our best efforts, a code with the scope and complexity of ATHLET will never be free of weaknesses or errors.

Released ATHLET versions are patched whenever it is necessary or appropriate. Patches are classified as

- **Critical:** Program errors are fixed which could significantly impair the quality of results or reliability of code application. In that case, all users will be informed via the ATHLET User Area. The user is strongly recommended to update his ATHLET version and recent results obtained with the previous code version.
- **Non-critical:** The code performance, predictiveness and/or user convenience are improved. Particular applications may require program updates which are not needed for usual applications.

Important known issues with the code and their resolution or applicable workarounds are summarized in section 2 of this document.

## 1 Program Updates in ATHLET 3.3

In this chapter, **bold face** indicates that user's action may be required even for existing input decks.

### 1.1 Thermo-Fluidynamics

- New evaporation model for mixture level with a more realistic consideration of impact of NC gases
- Modified ML condensation model
- Improved modelling of entrainment fraction (based on Pan-Hanratty) and of onset of entrainment for horizontal pipes
- 3D model: if TFO is part of a 3D (cylindrical) domain and annulus drift is specified in the input, pipe drift will be used instead
- Additional transport equations for solutes (mainly thought for analysis of zinc-borate issue after LOCA)
- Modelling of zinc release from internals (for gratings in containment)
- New vertical bundle drift option for small-size test facility bundle
- New gas components available: CO and CO<sub>2</sub>
- Special treatment of arising/vanishing phase (i.e. very small phase fraction) in momentum equation removed (subroutine D2MDZC)
- Updated thermodynamic properties of NC gases. In order to ensure consistency, specific gas constants are now calculated from molecular weights.
- If *reduced* input format under PW MIXLEVEL was employed, AMLSO and VMLTO weren't correctly interpreted. Fixed.
- Correction of evaporation rate due to overheated steam according to Sideman. Factor  $1 - \gamma$  omitted.
- Adaptation of boron transport model
- Calculation of flow losses in bulk condensation model corrected.

- Bug-fix in Double-end-break model. Model was not executable in previous code version.
- Modified formulation of so-called water-level force (2m)

## 1.2 HECU

- Flow instability ratio acc. to Whittle-Forgan as optional plot quantity (print level `IOUT0=4`) (mainly for research reactors)
- Cladding oxidation model extended for FeCrAl (ATF)
- New CHF correlation acc. to Sudo and Kaminaga, mainly for research reactors and fuel assemblies with narrow rectangular flow channels
- If wall temperature exceeds Leidenfrost temperature, a modified fluid reference temperature for calculation of heat transfer is employed
- Dedicated heat transfer correlations for thermosiphons acc. to Gross (condensation) and Imura (evaporation) implemented (selectable via input parameters `IHTC4L/R` and `HTC7L/R`, resp.)
- **Meaning of `TL0` (fuel rod pitch) extended to distinguish between square and hexagonal bundles** (e.g. required for Inayatov bundle factor)
- Special heat transfer correlations for laminar, wavy and turbulent film condensation within vertical tubes, selectable via input parameter `IHTC4L/R`
- Slightly modified calculation of transition boiling heat transfer in order to enable earlier rewetting for those HCVs that didn't reach film boiling before

## 1.3 Neutron Kinetics

- Additional thermal-hydraulic feedback reactivities available, mainly for LM cooled reactors: thermal cladding expansion feedback, thermal fluid or structure expansion feedback for any TFO or HCO

## 1.4 Numerical Solver

- NuT – if activated – is used during SSC as well

## 1.5 Component Models

- Condenser model with NC gases: Condensation of inflowing vapor is limited to saturation pressure at present liquid temperature.
- Separator model: For flooded separator and ML inside the dome, the distribution of carry-over steam mass flow is adjusted. Non-separated steam is directed to lower-most CV (below mixture level) of separator dome instead to separator exit branch.
- Separator model: The distribution of separated carry-under liquid mass flow below/above mixture level in separator outlet branch is corrected. Former implementation could result in (low frequency) oscillations of the mixture level in the separator outlet branch.
- **Injection model: injection angle  $ANGINJ$  for injecting TFO is limited to  $0 \leq ANGINJ \leq 180$ : (for ECCMIX injection:  $0 < ANGINJ < 180$ )**
- Time-Dependent Volume (TDV): New optional input ( $PW_{CORRLIMIT}$ ) to limit or skip pressure and enthalpy adjustments after SSC

## 1.6 GCSM

- New GCSM postprocessing signal (via  $CW_{POSTPRO}$ ): total fluid enthalpy in TFO
- Additional call of GCSM at the end of SSC to correctly set process signals related to NC gas quantities. Hence, all control signals will be updated too.
- **For CV with mixture level inside, the process signal type  $PRESS$  provides now the pressure in the center of the CV and no longer the pressure at mixture level elevation.**

## 1.7 Plug-ins

- New plug-in for water-steam material properties according to IAPWS-95 standard with increased accuracy mainly in the range of low pressure ( $\leq 1$  bar). Plugin is activated under  $CW_{PLUGIN}$  writing "sbt195" and is employed if light water is working fluid.
- **Initialization of plug-ins is shifted to the beginning of an ATHLET run, when  $CW_{PLUGIN}$  is read in**



- Additional non-boiling model working fluids added to plug-in MPEXT.
- MHTCEXT plug-in extended by additional interface for *forced convection heating to liquid* heat transfer regime
- Coupling via HCO-surface (e.g. with COCOSYS) improved
- Gain-factor for GCSM signals of type `EXTERNAL` no longer used
- ATHLET Water-Steam property package available inside plugin MHTCEXT
- CFD coupling interface expanded to NC gases
- To handle different 3D neutron kinetic code plug-ins in parallel, the naming convention for the according libraries was modified. The library name must start with “n3kin” and may be expanded additional characters, e.g. “n3kin\_dyn3d”.

### 1.8 General

- Restructuring of loops in routine DGZON to reduce CPU time
- Intel Fortran 19 compiler used for current release
- Restart format modified: old restart files will not run with current program version
- Jacobian coherency test implemented (developer tool): to be activated via environment variable `ATHLET_CHECK_JACOBIAN_COHERENCY` (for both MS Windows and Linux)
- Plot data for models NEUKINP, STEAMGEN and QUENCH are provided independently of HECU output amount (e.g. if `IOUTH0=0`)
- New print/plot data: flow regime information from both interfacial shear model as well as heat and mass transfer model
- `libadt.dll` is replaced by `libfde.dll`

### 1.9 GUI / Tools

- New python-based plotting tool ‘batchplot’ available
- Windows tools “Plot Variable by Excel” and “Excel to pd” no longer distributed due to license constraints

- Several minor bug fixes and improvements in AIG
- Visualization error of mixture level in ATLAS within pipes with more than eight CVs fixed
- Output of the two post-processing utilities “Select Plot Data” (for MS Windows) and “athpost” (Linux) adjusted and harmonized to each other: e.g. a headline with variable names is always printed and the number of records is given in the first column.

## 2 Known and Fixed Program Errors

Tab. 2.1 lists major known bugs and shortcomings that are existent in the current ATHLET program version. In addition, the program version where the respective error was detected first is given. However, the particular error may already be existent (but not found) in earlier code versions as well.

Tab. 2.2 gives an overview of the error fixes that are considered in the current ATHLET program version. Here, fixes are reported only to those errors, which did not cause an immediate program stop, but could result in a successful finalization of the calculation with possibly impaired outcome. In such cases, the error is hardly “visible” for the user. The description of all other bug-fixes is included in chap. 1 on program updates.

**Tab. 2.1** Known Bugs in the current program version

Bug Description	Existent since code version
<p><b>HCO Geometry: Assignment of HCV to wrong CV of coupled TFO</b></p> <p>Error may occur for non-parallel HCO and TFO (e.g. in heat exchangers secondary side). Depending on the specific geometry, a possible workaround is partition of TFO (and HCO) into several shorter objects each coupled to the associated HCO along the appropriate length. Thus, the assignment of CV and HCV is done more or less manually in the input deck.</p> <p>Measure in code: Extended input checks to detect assignment error and inform user.</p>	3.1A (and former versions)
<p><b>Multiple parallel channels with MLs: Numerically unstable behavior</b></p> <p>Particularly for parallel channel models, multiple parallel MLs can behave unstably and currently should be avoided at least for pool boiling situations. Numerical issues may also lead to unphysical behavior. Parallel mixture levels repeatedly transitioning CV boundaries at same elevation can also impair numerical efficiency.</p> <p>Measures: For pool boiling situations a final solution is not available. In general, the ML transition criteria can be optimized, or the CV boundaries can be changed so that (slow) ML transition is avoided.</p>	3.2 (and former versions)
<p><b>Supercritical CO<sub>2</sub> property package:</b></p> <p>Properties are available in the range 73.773 bar &lt; p &lt; 300 bar and 283 K &lt; T &lt; 675 K. Accuracy deteriorates in the neighborhood of the critical point, therefore it is <u>not</u> recommended to use the data below 90 bars and 42 °C (315 K).</p> <p>Measures: The mass balance should be checked carefully.</p>	3.2

<p><b>Program abortion due to low pressure</b></p> <p>It was found, that ATHLET sometimes stops because pressure falls below lower limit of water-steam property package. The problem occurred in CV with significantly subcooled liquid, e.g. in the ECC injection pipe, and during phases with pressure disturbances, e.g. connected to high condensation rates somewhere inside the coolant system. Reasons may be too small/late evaporation (at low vapor saturation pressure) or uncertainties in the material properties at low pressures. The problem is under investigation.</p> <p>Measures: Modify nodalization of the region where the problem occurs.</p>	<p>3.1A</p>
<p><b>Form losses and turbulence model in 3D model:</b></p> <p>Optionally, viscous shear stresses and turbulent friction can be considered in momentum equation of 3D model by activating an in-built zero-equation turbulence model (only reasonable for highly resolving meshes). Consequently, for wall-distant junctions the standard wall friction is no longer employed. In addition, form losses are also not calculated. This may be not desired or even erroneous in the case of small-scale internals (not resolved by the numerical grid) and form losses automatically introduced by ATHLET to compensate for pressure recovery due to increasing flow area along a junction.</p> <p>Measures: None. Use 3D model without turbulence model (recommended approach for grids with large scale CV).</p>	<p>3.1A</p>

**Tab. 2.2** Error fixes for the current program version

Error Title	Error description and taken measures
Flooded separator and carry-over steam and gas flows	<p>For a flooded separator, separated steam was transported via the carry-over junction towards the separator exit branch instead towards the dome. Subsequently, steam could also enter the steam generator downcomer. With the provided correction, separated steam is always transported to a CV inside the separator dome (possibly below mixture level inside the dome, depending on elevation of flooding) in case that separator is flooded.</p> <p>For a flooded separator, the energy flow connected with non-condensable gas flow through carry-over junction towards the dome was not considered. This is also corrected with the new implementation.</p>
Flow losses in bulk condensation model	<p>The bulk condensation rate depends on several parameters, among them the frictional losses. Due to a programming error, the friction loss was overestimated for some applications, resulting in an overestimated condensation rate. The error was fixed. In addition, the method for the calculation of the friction loss inside the condensation model was harmonized with the approach used in ATHLET's friction loss model (see Models &amp; Methods Manual).</p>
Reduced input for mixture level model	<p>According to the input description, ATHLET accepts reduced input for the mixture level under PW MIXLEVEL. If reduced input was given, AMLSO and VMLTO were not correctly assigned to the respective mixture level. Instead, default values were used. The implementation was corrected.</p>

### 3 Patches for ATHLET 3.2

The following lists the ATHLET program patches for the release version ATHLET 3.2.

In this chapter, **bold face** shows the chief cause of releasing a new ATHLET patch (if there is one). Others are program improvements provided on occasion of patching ATHLET to improve overall code performance for both users and developers.

#### 03.06.20 ATHLET 3.2.1 released

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##### Non-critical patch

03.06.20 New (optional) hardware-action to control point-kinetics rod power during zero-transient calculation. This option facilitates establishment of an asymmetric core power distribution, e.g. by initially specifying a homogeneous power distribution (also for the connected steam generators) and by adjusting this power distribution via GCSM during zero-transient.

Modified (optional) input data under PW RODCON:

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Input:

IQF10 AIQF10 AIQF20 IPOWM0 IPOWL0 QROD0 QROD00 FPROD **opt. :AQROD0**

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AQROD0: Optional input: Name of GCSM signal controlling relative rod power during zero-transient calculation (100% power: QROD00)

19.05.20 Bug fix for Dobson-Chato heat transfer correlation (condensation in horizontal tubes). Transition criterion between stratified and annular flow included an error.

27.03.20 Extended error checks for PW BRANCHING:  
Branching data provided twice for one TFO (e.g. for a SJP connecting two branch objects) are checked for consistency

26.03.20 New process signals TMTCORE (average temperature of in-core melt) and LPTWOAVE (average outer surface temperature of the lower plenum [K]) are available (ATHLET-CD).

- 17.03.20 Spray model: print and plot variables GAMDRO and HTCOUT were not properly set.
- 24.01.20 Mismatch between Jacobian matrix structure (representing the thermal-hydraulic network structure on a matrix level) and the actual dependencies of solution variables according to physical modelling resolved. Comparing the patched code version with the original release version 3.2, this may cause (numerically) different results in cases where separator model, injection model, 3D model or the flag I2MFTRX=1 is used. ISFTRX is always set to one now.
- 18.12.19 Additional trigonometric functions available under CW PARAMETERS:  
arcsin, arccos and arctan
- 12.08.19 Bug-fix in selection of heat transfer correlation for film boiling. Selection of Condie-Bengston correlation via input parameter IHTC1L/R resulted in program error.
- 12.08.19 Extended error checks w.r.t. priority chains provided by user
- 12.08.19 sCO<sub>2</sub> properties: Error in calculation of partial derivatives fixed

## 4 Program Updates in ATHLET 3.2

In this chapter, **bold face** indicates that user's action may be required even for existing input decks.

### 4.1 Thermo-Fluidynamics

- Evaporation and condensation (hence two-phase state) of working fluid sodium enabled.
- **New correlations for approximation of LM properties implemented. This requires enthalpy values for fills and TDVs different to those of A3.1A (s. M&M)! Recommendation: Calculate the enthalpy from p and T using the GCSM controller PROP.**
- New working fluids:
  - Supercritical carbon dioxide
  - Molten salts FLINAK, FLIBE
  - User-provided simple (non-boiling) working fluids
- 3D-model extended by ML capability
- Junctions branching off from a ML track may now be vertical, too.
- **Explicit drift flux model is no longer applicable.**
- New model for condensation-induced water hammer.
- **CW BORTTRANS: name of tracked solute has to be input, IBDEB<0 no longer valid;** own table of maximum solubility may be provided.
- **CW OBJECT: PW EVAPORATE no longer valid;**
- **CW MISCELLAN: AA must be 0.0!**
- New options to reduce / mitigate pressure wave propagation during zero-transient calculation (s. Input Data Description; CW ZEROTRANS).



## 4.2 HECU

- Modification of DNB calculation: DNB only dependent on CHF and no longer on minimum film boiling temperature. Min. film boiling temperature still used for onset of stable film boiling (end of transition)
- Radiation model extended: Simple treatment of radiative heat exchange between HCO surfaces and the environment realized. As a side effect, a new keyword TFO has to be input for the application of the already existing TFO-related radiation model in order to distinguish between both models (radiation to the environment and TFO-related radiation).
- MASL calculation:
  - MASL calculation starts from beginning of transient calculation.
  - ASL0 and THM0 used in SCAT method are now calculated by ATHLET (Input data ASL0 and THM0 are only used as starting values for stationary iterations.)
  - MASL calculation is stopped if core mass flow approaches zero.
- Heat exchanger model: New option IQHTX=2 for adaptation of heat transfer profile only
- Quench front model applicable for pressure < 50 bar (formerly: 30 bar).
- Calculation of fuel pellet center temperature modified (extrapolation from inner layer to center of cylinder).
- Print / plot output extended:
  - HCORS: total enthalpy stored in materials of any type of rod (reference temp. = 20 °C)
  - ISURFM: HCV index where max. surface temperature occurs
  - Single and total rod surface area (print)
  - Single and total heat exchanger surface area (print)
  - Heat flux in RODLEVEL and CORESUM (plot and print): QACOR, QACORS, QACORM
  - Linear heat generation rate LHGR per rod in W/cm (plot and print)

## 4.3 Neutron Kinetics

- 3D neutron kinetic codes coupled as plug-in (QUABOX/CUBBOX, DYN3D, PARCS)

#### 4.4 Numerical Solver

- Monitoring of increments of solution variables extended (s. CW INTEGRAT, PW DEBUG)
- Numerical Toolkit (NuT) plugin enables usage of scalable solver packages PETSc or MUMPS (see separate documentation)

#### 4.5 Component Models

- Separator-model: Corrected enthalpy flow rates across carry-under/over junction for cases with NC gases.
- New heat exchanger option for SSC: IQHTX=2 iterates heat exchanger power profile but doesn't adapt heat exchanger surface
- CDR1D tables are tagged in input file. New generation of tables is automatically triggered when required.
- CONDRU is now available as plugin (no longer implemented in ATHLET).

#### 4.6 GCSM

- **As GCSM block name (BLNAME), following expressions are no longer valid:**  
AIDA, BLOCK1, COCOSYS, COMPARATOR, CONDRU, CORESUM, COUNTER, DECAY, DT2, GENERAL, HEATHEX, INTEGRAL, LEVEL, MASSLOSS, MONITOR, PIPE, PI\_REGLER, SETPOINT, TFDGENERAL
- Deprecated models removed from GCSM library (boron tracking, homogeneous volume, accumulator model, containment model, SG level control)
- New process signals TSURFMAX, RELOMET, RELOCER, LPDISMASS and LHGR available.
- Process signals may be directly derived from 'visible' global variables, which are provided for every CV or HCV.
- Print/plot output
  - of GCSM signals can be controlled (CW OBJECTCON, PW GCSM)
  - GCSM hardware actions are compiled under block name HW-ACTION

#### 4.7 Plug-ins

- All plug-ins must be activated under CW `PLUGIN`.
- New plug-in for XL correlations (MASL method).
- New plug-in for CHF correlations.
- New plug-in for user-provided simple (non-boiling) working fluids.
- BOP model has to be provided as plug-in (example available)
- Watchdog plug-in to trace the stability of an ATHLET run and terminate the simulation in case that predefined critical conditions are hit.

#### 4.8 General

- **Modified ATHLET start parameters:** two parameters are mandatory: input file name and run identifier. Problem-ID, -rd, -r etc. deprecated. (see User Manual)
- CW `TOPOLOGY`: Input value `ISYS0` (index of fluiddynamic system – integer) changed to `ASYS0` (name of fluiddynamic system – string). The same holds for `AMCSYS` (former `IMCSYS`) under CW `MULTICOMP`.
- New sample case “VVER-1000” (generic)
- New simple sample: ATHLET “egg boiler”
- A line of the input file may consist of up to 720 characters
- ATHLET code structure:
  - ATHLET `exe`-file is mini executable that invokes the ATHLET shared library.
  - Core-degradation (ATHLET-CD) is now a plug-in invoked by ATHLET (if required)
- Generation of HTML-output requires start parameter `-html` (`HTML ON/OFF` in input file deprecated). HTML-output format revised.
- Command `PRINT ON/OFF` (first row of input deck) is now start parameter: `-printon`
- New output file `*.log`: contains major information of simulation run and input listing

- Number of new hooks for ATHLET simulation control by external program (see Programmer's Manual)
- Changeover from Fortran-77 to Fortran-90 (\*.f90)
- Max. number of generated restart data sets via ISREST, EXT coupling and signal handler: 10000. Beware of .re file size!
- CW REDEFINE: Some quantities may be redefined for all junctions (and not only for a single junctions) of a TFO.
- Several error messages improved.
- New Intel and GNU compilers applied: Release version generated with Intel 16.4.
- **Input and run time checks extended, e.g.:**
  - IPRI0/=1 no longer valid for PCs containing CVs. The steady state pressure distribution in the simulation system is not a free input data; must be calculated by SSC!
  - Heights of TFO and related HCO are checked for consistency.

#### 4.9 GUI / Tools

- Optionally, plot data may be generated in Hdf-5 format (instead or in addition to pd-format). Requires activation of Hdf-5 plug-in.
- New, platform independent GUI to start AC<sup>2</sup> calculations (including couplings and NUT). As an interim approach, the former ATHLET GUI is still applicable to run ATHLET utilities.
- ATHLET Input Graphic extensively revised (AIG-2)

## 5 Patches for ATHLET 3.1A

The following lists the ATHLET program patches for the release version ATHLET 3.1A.

**Bold face** shows the chief cause of releasing a new ATHLET patch (if there is one). Others are program improvements provided on occasion of patching ATHLET to improve overall code performance for both users and developers.

### 03.05.18 ATHLET 3.1A Patch #04 released

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- 01.05.18 New GCSM process signal type `PSTAGE`: provides power generated in the selected stage of the turbine set in [W].  
Example: `SPV0=5`. would be stage 5 of the turbine set related to `OBJNAM`.
- 25.03.18 Auto activation for plug-ins. If a compatible plug-in is present in `bin/plugin`, its procedures `initialize_c` and `execute_c` will be automatically called by ATHLET.
- 08.03.18 Improved error bounds for ML mass fraction as well as demand of additional Jacobian updates after ML transfer reduce unreasonable high mass error which may occur in cases of very fast ML movement.  
=> Restart files of former ATHLET runs are no longer applicable!
- 07.03.18 New Hooks available, please see Programmer's Manual, chapter 4.3
- 05.03.18 Libadt update. Please use `connectCallback` instead of `setCallback` if you are using hooks with a FORTRAN code. Python is not concerned thanks to an alias.
- 08.02.18 New GCSM process signal type `LPDISMASS` available (total mass discharged from lower plenum; module AIDA)
- 29.01.18 ML transition: If iteration of ML quantities did not converge for a falling ML, `XQMO` (above ML) is set to former value (may improve stability).  
`IGAM0` controls now the reduction of mass exchange rates at low void fraction, too.  
Up to now, this was always active. Hence, reduction can now be switched

off.

GCSM: All hardware actions are now available in the plotting data under Block Name `HW_ACTION`.

New input data checks added.

- 18.12.17 New GCSM process signal type `RODSEGPOW`: provides power generated in one single HCV of a rod component.
- 08.11.17 Modification of multiplication factors for uncertainty analyses `OFI2H`, `OFI2V`. The two-phase flow multipliers were corrected. Currently, they are void fraction dependent. For single phase water flow, the factors written in input are transformed to value 1.
- 13.10.17 Edit input-reading procedure to pass any extra argument through a new scope. In order to get a non-ATHLET argument and its value, please use:  
`arg_scope => getScope (root_scope, 'global', 'arglist')`  
!get input parameter *argname* (in this case, a string)  
`parameter_input = char(string(get(arg_scope, '-argname')))`
- 11.10.17 Libadt has been updated from 2.5 to 2.6 without any effect on calculation results. Please change the properties for the linker, if you are building your own plugin.
- 22.08.17 Correction for direct heating using coupled simulation with 3D-kinetics

- 18.07.17 ATHLET 3.1A Patch #03 released** \_\_\_\_\_  
**Non-critical patch, however module CONDRU was not correctly compiled in Patch #02 for Linux application**
- 05.07.17 1M model: Limitation of |relative velocity| to < 100 m/s  
Reason: Relative velocity can increase very fast while the limitation through entrainment is damped via time lag; this may lead to numerical problems.
- 29.06.17 Module CONDRU compiled and linked with correct compiler option "save all variables"
- 28.06.17 New process signals TSURFMAX, RELOMET and RELOCER available  
TSURFMAX: Max. surface temperature in core  
RELOMET: Relocated metallic mass (ECORE module)  
RELOCER: Relocated ceramic mass (ECORE module)
- 22.06.17 New control of print/plot output of GCSM signals:  
Needs additional input data under CW OBJECTCON after PW HCO:

#### GCSM Signal Control Data (PW GCSM)

This PW is only to be input if the general control data shall be overwritten for the GCSM signals.

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#### Input:

IOUTG0

#### If desired:

YNAME            IOUTG

:            :

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#### Explanation:

IOUTG0: Controls output of GCSM signal values:  
=0: No signal is output (except problem time signal)  
=1: All signals are output

YNAME: GCSM signal name

IOUTG: Controls output of signal YNAME (s. IOUTG0)

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**31.05.17 ATHLET 3.1A Patch #02 released****Non-critical patch**

- 12.05.17** Correction of restart structure for scoop in combination with gas-release.  
**Restart-Files are no longer compatible with patch#01.**
- 20.03.17 Binaries are now tagged with SVN-version and compiler information
- 08.03.17 New check of validity of CDR1DIN input data
- 06.03.17 Callback hook IDs modified (see Programmer's Manual)
- 06.03.17 Additional retrace trigger via visible scope-variable *retrace\_request\_idx* in module CAOR (dll-Version only)
- 16.02.17 Balance of Plant (BOP) models can be used as plugin
- 14.02.17 'Explicit' drift model ( $J_{DRIFT} > 10$ ) is no longer valid; → program stop  
Lengths of input character strings must be  $\leq 10$ ; → program stop  
Specific heat of graphite: error for  $T > 1500$  K fixed
- 17.01.17 New WATCHDOG plugin to "early-terminate" ATHLET if one or multiple critical conditions are attained. These conditions can be formulated as GCSM signals. Based on the employed watchdog function, the supervision can be permanent or temporarily enabled during the computed time.
- 13.12.16 MASL calculation is stopped if core mass flow approaches zero.  
CDR1D table in input deck is tagged now with date of generation and used ATHLET program version; new tables will be generated when Patch#02 is applied first.
- 17.11.16 Start of a ML in CVs with (pure) NC gas improved  
Condensation at ML surface in presence of (pure) NC gas improved  
Quench front model applicable already at  $p < 5$  MPa (former 3 MPa)  
Length of plot array is printed in .out file



**08.11.16 Coupling of 3D neutron kinetics codes with ATHLET is done now exclusively via plugin technique. The 3D neutron kinetics code has to be provided by the user as DLL or shared library, resp.**

New input data check concerning definition of priority chains of autonomous systems

Processing sequence improved to enable identical results of serial and parallel execution of ATHLET

Several bugs / shortcomings of plotting package fixed

Print 'ARTIFICIAL EVAPORATION...' does not longer appear for discharge junctions (JTYP=5)

Distribution of 64 bit code version only (32 bit version can be provided on request)

Intel Fortran compiler option "Floating Point Speculation" changed from *fast* to *safe*

Linux code version: change of Intel Fortran compiler from version 15.3 to 16.4

Several input / program checks improved / extended.

We recommend the download of the complete setup file and to re-install ATHLET.

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- 15.07.16 ATHLET 3.1A Patch #01 release** \_\_\_\_\_  
**Non-critical patch**
- 14.07.16 Improved import and print-out of input OMP-settings (PW PARALLEL)
- 13.07.16 New error check for inconsistent input data: BRANCH2M coupling (i.e. JDPA=2) no longer possible for junctions, of which JDPA is set equal zero by BRANCHING data
- 12.07.16 Unix GUI, tool "Plot by plx file": error in file selection dialog corrected
- 06.07.16 New tool to convert .plt to .plx files.
- 05.07.16 A GCSM summary is printed including number of loosely and closely coupled signals, external signals, etc. (s. NUMBER OF GCSM SIGNALS)
- 05.07.16 TFO component 'condenser' (ICMPO=4) may be a copy of standard TFO and vice versa.
- 04.07.16 Module CDR1D: Control of automatic update of CDR1D tables improved. It completes checks and avoids unnecessary updates.**
- 29.06.16 Speed up of FEBE equation solver (identical results)
- 29.06.16 Discontinuity in calculation of HTC<sub>MIC</sub> removed; may speed up simulation
- 28.06.16 athlgo considers wall time and number of CPUs (OMP parallel execution of ATHLET) when limiting MCPU.
- 28.06.16 Check of external GCSM signals only on demand; may speed up simulation significantly if a very large number of GCSM signals is defined**
- 24.06.16 Improved readability of TIME INTEGRATION SUMMARY print output for long term simulations (> 100000 time steps)
- 08.06.16 Check concerning applicability of quench front model (p < 30 bar) improved.

- 19.05.16 Parameter list of interface routine `MHMASL` includes now annular flow length, too. MASL calculation starts now at begin of transient calculation. Start values for transient MASL are no longer input data but results of stationary MASL.